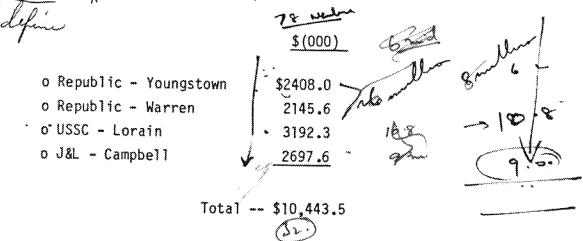
### Cost-Effectiveness Analysis of Ohio Quench Tower Pollution Control Options

Cost-effectiveness (C-E) ratios will be derived for three control options; multiple row baffles, clean water quenching (TDS of 1500 mg/l) and combined multiple row baffles and clean water quenching. The pollution reduction and cost of control for each option are computed for J&L - Campbell, RSC - Warren, RSC - Youngstown, and USSC - Lorain.

The C-E ratio is the total annualized cost of control divided by the annual reduction of pollution. The total annualized cost has two components; annual capital recovery (financial) costs, and annual operation costs.

The costs of clean water quenching for the four Ohio plants were computed from the development document for the effluent limitation guidelines for Iron and Steel. The capital cost of wastewater treatment is based on the size of the facility needed to treat the waste ammonia liquor from by-product cokemaking operations, allowing the quenching water to reach 1500 mg/l TDS. The capital costs for clean water quenching for each plant are:



The total annualized cost is 22.8 percent of the capital cost of clean water quenching. The methodology used to compute this percentage is the present value cash flow method (see table A).

The annual operation costs for clean water quenching include the following costs (from Iron and Steel development document):

- Operation and Maintenance

- Energy and Power

- Land

- Steam

- Sludge Disposal

- Waste Acid

- Hazardous Waste Disposal

- Chemical

- Oil Disposal

- Crystal Disposal

As a percentage of capital cost, the annual operation cost is 17 percent.

TABLE A

## Annualized Cost of Clean Water Quenching (example investment of a \$1000.00)

	1	]	2]	3]	4	] 5]	] 6]	7]
Useful Life	Operation	n		Equity	Debt	Depre-		
(# of years)	Costs	•••	<u>ITC</u>	<u>Finance</u>	<u>Finance</u>	ciation	NCF	MPV
0		+	100	-650			-550	<b>-</b> 550
The state of the s	-85				-70.9	+69.8	-86.1	-83.0
2	-85				-65.9	+95.2	-55.7	-51.8
3	<b>-</b> 85				-61.3	+84.5	-61.8	
4	<del>-</del> 85				-57.1	+78.6	-63.5	-54.9
5	<del>-</del> 85				-53.1	+73.1	-65.0	-54.2
6	<del>-</del> 85						-85.0	-68.3
•	*							~ · ·
*	*						•	
•	*						*	
*	*						•	
25	-85						-85	-34.1

NPV of Investment -1835.8 over Useful Life

Post-tax annualized cost - \$114.1

Pre-tax annualized cost - \$228.2 (assumed marginal tax rate of 50.1%)

Pre-tax annualized cost or a percentage of capital cost is 22.8 percent.

#### Footnotes to Table A:

1. Post-tax operation cost is 8.5% of capital cost (assumed marginal tax rate of 50.1%) and left operation costs in real terms.

#### (Table A continued)

- 2. Investment tax credit of 10% from Economic Recovery Act of 1981.
- 3. Steel Industry will finance capital investments with approximately 65% equity funds and 35% debt; data from FTC's Quarterly Financial Report.
- 4. Used post-tax weighted cost of capital of 4.46%, see TBS's economic analysis of effluent guidelines for Iron and Steel. Debt payments are put into real terms using a 7.5% inflation factor.
- 5. Depreciation schedule from Economic Recovery Tax Act of 1981, depreciation in post-tax and put in real terms using a 7.5% inflation factor.
- 6. Net cash flow which is the sum of the rows in Table A.
- 7. Net Present Value of the cash flow using a discount rate of 3.72% that includes an inflation rate of 7.5% (calculated from Chemical Engineering plant cost index) and 11.5% rate of return on equity (calculated from FTC's QFR).

An option to be considered is the treatment of all wastewater used in quenching, bring the TDS concentration in the quench water down to 500 mg/l. The incremental capital cost and annualized cost are the following:

	Capital Cost	Annualized Cost
	<u>\$(000)</u>	\$(000)
Republic-Youngstown	1523.2	347.3
Republic-Warren	2031.9	463.3
USSC-Lorain	3055.4	696.6
J & L-Campbell	2508.6	<u>572.0</u>
Total	- 9119.1	2079.2

#### (Table A continued)

Using the functions in Table \_\_\_\_\_ to calculate the pollution reduced from multiple row baffles and water at 1500 mg/l TDS to water at 500 mg/l will yield the following C-E ratios:

	\$ Per Ton of TSP Reduced
Republic - Youngstown	\$5890
Republic - Warren USSC - Lorain	\$8740
	\$8100 - \$7300
J & L - Campbell	<b>\$</b> 8540 <b>- \$</b> 8060
Aggregate	\$7640

The annualized costs of clean water quenching (1500 mg/l) for each plant are:

_	\$(000)
Republic - Youngstown	549.0
Republic - Warren	489.2
USSC - Lorain	727.8
J&L - Campbell	<u>615.1</u>

Total --- \$2381.1

The capital cost of multiple-row baffles for quench towers at the four Ohio Steel plants was estimated by a contractor, and these cost estimates are consistent with the installed capital cost of multiple-row baffles used in the draft NSPS for quench towers and with estimates developed by J & L (memo from W. Wilson of J & L to J. Kunz of Region III, dated 4/21/82). Multiple-row baffle capital costs for each plant are:

(Table A continued)

	<u>\$(000)</u>
Republic - Youngstown	400.0
Republic - Warren	400.0
USSC - Lorain	760.0
J & L - Campbell	820.0*

The operating costs for baffles are negligible, and these costs were assumed to be zero. Total annualized costs for multiple-row baffles will include annual capital recovery costs and, because baffles have a four year useful life, a periodic replacement cost. To compare properly the costs and pollution reductions from different control options, the time period for each option must be equal. Because an investment in wastewater treatment has a useful life of 25 years, to compare costs/benefits of baffles with clean water quenching, the cost of baffles must also be calculated over a 25 year period. Using the same methodology and financial assumptions will yield a total annualized cost for baffles as a percentage of capital cost of 20.8 percent (see Table B).

TABLE B
Annualized Cost of Multiple-Row Baffles
(example investment of \$100.0)

Time	Finance	Debt		Replace-	1)		
Period IT(	by Equity	<u>Finance</u>	<u>Depreciation</u>	ment Cost	NCF	NPV	
0 +10	<b>-</b> 65					***************************************	
1		-11.4	+11.6	990	-55.0	-55.0	
2		-10.6	+16.4	***	+ 0.2	+ 0.2	
3		- 9.8	+14.9	***	+ 5.8	+ 5.4	
4				***	+ 5.1	+ 4.6	
5				900pi	0	0	
ZZZZZZZ				-40.0	-40.0	-33.3	
				1	1		
						1	
					•	1	
25	*			I	1	0	
				Total	=	-171.9	
						-1/1.3	

\*J & L's cost estimate to install Carl Still baffles at their Campbell quench towers, but the towers at Campbell have multiple-row baffles; therefore, for the purposes of this study, J & L baffle cost will not be used in the C-E analysis. Post-tax present value annualized cost - 10.7

Pre-tax present value annualized cost - 21.4

Annualized cost as a percentage of
 capital cost - 21.4%

Footnote: 1) Useful life of baffles is four years, however, replacement cost is approximately 40 percent of original capital cost and would not be treated as a new capital expenditure in production control, but as a maintenance expenditure.

The annualized costs of multiple-row baffles for each plant are:

	\$(000)
Republic - Youngstown	85.6
Republic - Warren	85.6
USSC - Lorain	162.6
J & L - Campbell	this spir age

Total --333.8

Taking the emission reductions for each pollution option from Table 8 and dividing the reduction into the appropriate annualized cost will yield the C-E ratio for that control option.

The C-E ratios for requiring clean water Aquenching and status quo baffles are:

	\$ Per Ton of TSP Reduced
Republic - Youngstown	<b>\$</b> 390
Republic - Warren	\$420
USSC - Lorain	\$740
J & L - Campbell	\$710-\$530
Aggregate	\$530

The C-E ratios for requiring only multiple-row baffles are:

	\$ Per Ton TSP Reduced
Republic - Youngstown	\$100
Republic - Warren	\$120
USSC - Lorain	\$510-\$140
J & L - Campbell	Main voter doc
Aggregate	\$140

The C-E ratios for requiring multiple-row baffles and clean water quenching are (incremental cost of clean water):

	\$ Per Ton TSP Reduced
Republic - Youngstown	\$900
Republic - Warren	\$980
USSC - Lorain	\$910-\$610
J & L - Campbell	\$710-\$530
Aggregate	\$760

Attachment 0

In order to determine the range of particulate emissions from the three (3) J&L quench towers, Aliquippa No. 3, and Campbell Works Nos. 4 and 5 when operating with 1500 mg/l TDS quench water, the following information and equations were used. In addition, each tower has certain "other" factors that may affect these estimates and are outlined in the text.

To determine the TDS quench factor equation, I used:

$$\frac{\text{(1)} \quad \underset{\hat{k}}{\text{mg}} \quad \text{x} \quad \overset{\hat{k}}{\text{x}} \quad \overset{1B}{\text{xmg}}}{\text{gal} \quad \text{mg}} \quad \text{x} \quad \frac{\text{Quench}}{\text{t} \quad \text{coal}} \quad \text{x} \quad \frac{\text{gal. water loss}}{\text{quench}} \quad = \quad \text{1BTDS/t coal charged}$$

To determine the emission (particulate) factor:

(2) 
$$\gamma = 0.19 \times +0.56 - (APCA Paper Fig. 4-Front Half)$$

(3) Emissions = .35 lb t coal per 1000  $\frac{mg}{\tilde{k}}$  TDS (APCA Fig. 3 Carv Emissions Dat

For Aliquippa No. 3 tower then using equations 1 & 2:

$$\frac{1500 \text{ mg}}{\ell} \times \frac{3.785}{1} \times \frac{1}{454,000} \times \frac{1}{30.7} \times \frac{(110 \cdot 30.7)}{1} = 1.38 \text{ lBTDS/t coal}$$

$$Y = 0.19 (1.38) + 0.56$$

Y = 0.82 1B particulate/t coal

Using equation 3

$$Y = \left(\frac{.35}{1000} \times 1.5\right)$$

$$Y = .52$$

The baffles in this tower are not very effective due to the spacing left between each slat and the use of only one row. The loss of 110 gallons per ton of coal is believed excessive and the estimated loss is thought to be 90-1-0 gals per t. coal. This tower may be testable.

Campbell No. 4

EQ. 1 
$$\frac{1500 \times 3.785 \times 1881}{454,000 (17.1)}$$
 gals = 1.38 lBTDS/t.coal

EQ. 2 
$$Y = .19 \times +0.56$$
  
 $x = 1.38$   
 $Y = 0.82$  1B particulate/t.coal

EQ. 3 
$$Y = \frac{.35}{1000} \times 1.5$$
  
 $Y = 0.52$ 

Towers No. 4 and 5 have four rows of baffles and a loss rate of 110 gals/t. coal is not considered possible.

Nor should the same emission factor be applied due to use of a more effective baffle arrangement. These towers are not testable.

# UP-STACK WATER FLOW AS EXTRAPOLATED FROM CYCLONE AND IMPINGER CATCH

Location	Test Type		Gallons - Up-Stack		
			Average	Range	
Lorain	Clean		1649	874-2212	
	Dirty	Combined Avg.	1895 1767	1054-2459 874-24 <b>5</b> 9	
Dofasco	Clean		1605	587-2964	
Gary #3	Clean		2577	2230-2804	
	Dirty O	Combined Avg.	$\frac{2347}{2462}$	2144-2748 2144-2804	
Gary #5	Clean		1240	1076-1396	
	Dirty	Combined Avg.	$\frac{1189}{1214}$	1115-1265 1076-1396	

Water Loss Rate Gals/t. Coal Charged

Lorain	135
DOFASCO	100
Gary 3	70
Gary 5	301

Emission Rate when water loss is estimated to be 95 gals/t. coal

Campbell Towers 4 and 5

Eq. 1 
$$\frac{1500 \times 3.785 \times (95 \times 17.1)}{454,000 (17.1)} = 1.19$$

Eq. 2 
$$y = .19 (1.19) + .56$$

Emissions = 0.79 lbs. particulate/t. coal charged

Since none of these numbers can be used as definitive answers to the quench tower emission rate question, a range for each of the three towers is presented below. It is solely a questimate of particulate emissions based on past experiences and is thought to be representative of results from an actual sampling program.

Emissions (lbs particulate/t. coal, front half only @ 1500 mg/l TDS)

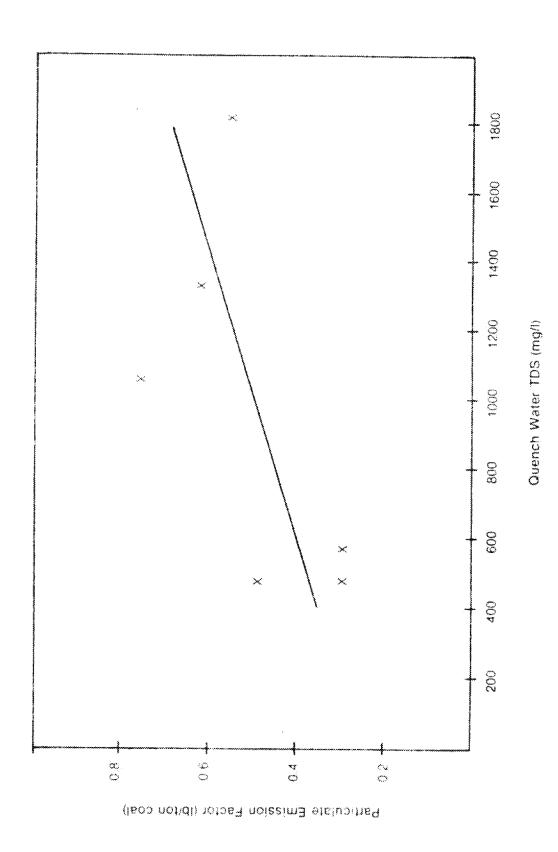
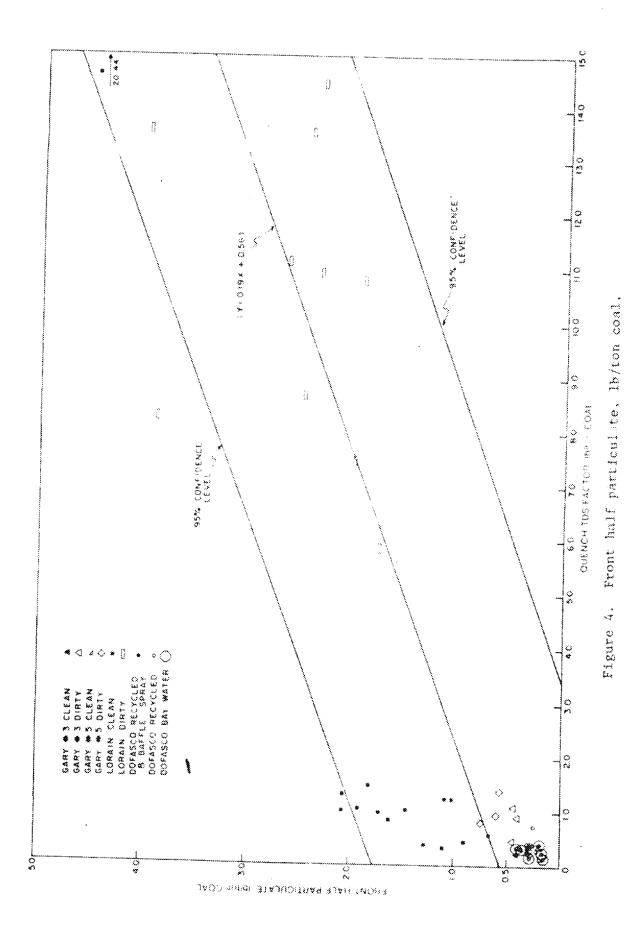


Figure 3. Gary emissions correlation.



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